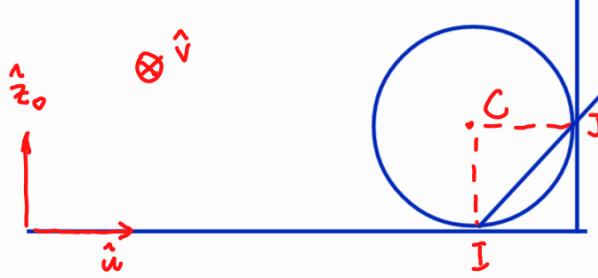


## Exam 2



(Q.1)

Position of C is given by

$$\underline{r}_{OC} = R \hat{u}$$

Take  $\frac{d}{dt}|_0$  to find  $\underline{\nu}_{C/I_0}$ , using

$$\frac{d}{dt} \hat{u} = \dot{\theta} \hat{v} \Rightarrow \underline{\nu}_{C/I_0} = R \dot{\theta} \hat{v} \quad (1)$$

We also know that  $\omega_{I_0} = \omega(\hat{u} + \hat{z}_0)$  (see sketch) since instantaneous axis must pass through both I and J (no slip is imposed). This gives another way to find  $\underline{\nu}_{C/I_0}$  to relate  $\omega$  to  $\dot{\theta}$ :

$$\underline{\nu}_{C/I_0} = \underbrace{\underline{\nu}_{IG/I_0}}_0 + \omega(\hat{u} + \hat{z}_0) \times \underbrace{\underline{r}_{IC}}_{r \hat{z}_0} = -r\omega \hat{v} \quad (2)$$

Compare (1) and (2) to find  $\omega = -\frac{R}{r} \dot{\theta}$ .

We conclude with the expression of the kinematic screw of body 1:

$$\{\mathcal{N}_{I_0}\} = \begin{cases} -\frac{R}{r} \dot{\theta} (\hat{u} + \hat{z}_0) \\ R \dot{\theta} \hat{v} \end{cases} \quad \text{(resolved @ C)}$$

(Q.2.)

We take  $\frac{d}{dt}|_0$  of  $\underline{\nu}_{C/I_0} = R \dot{\theta} \hat{v}$  to find

$$\underline{\alpha}_{C/I_0} = R(\ddot{\theta} \hat{v} - \dot{\theta}^2 \hat{u}) \quad (3)$$

where we use  $\frac{d\hat{v}}{dt} = -\dot{\theta} \hat{u}$ .

$$\text{Also } \underline{\alpha}_{I_0} = \frac{d}{dt}|_0 \omega_{I_0} = -\frac{R}{r} \ddot{\theta} (\hat{u} + \hat{z}_0) - \frac{R}{r} \dot{\theta}^2 \hat{v} = \underline{\alpha}_{I_0} \quad (4)$$

(Q.3)

We have linear momentum  $m \underline{\nu}_{C/I_0} = m R \dot{\theta} \hat{v}$ .

To find angular momentum about C, we use  $\underline{H}_C = \underline{I}_C(\omega_{I_0})$ .

We do not need a basis to find this expression (for a sphere)

$$\text{We get } \underline{H}_C = \frac{2}{5} mr^2 \omega_{I_0} = -\frac{2}{5} mr R \dot{\theta} (\hat{u} + \hat{z}_0).$$

We conclude with the expression of  $\{\mathcal{H}_{I_0}\}$ :

$$\{\mathcal{H}_{I_0}\} = \begin{cases} m R \dot{\theta} \hat{v} \\ -\frac{2}{5} mr R \dot{\theta} (\hat{u} + \hat{z}_0) \end{cases} \quad \text{(resolved about C)}$$

(Q.4)

With the expression of the action screw

$$\{\mathcal{A}_{I \rightarrow J}\} = \underbrace{\begin{cases} -mg \hat{z}_0 \\ 0 \end{cases}}_C \text{ gravity} + \underbrace{\begin{cases} N_I \hat{z}_0 + F_{In} \hat{u} + F_{Ir} \hat{v} \\ 0 \end{cases}}_I \text{ contact @ I} + \underbrace{\begin{cases} -N_J \hat{u} + F_J \hat{v} \\ 0 \end{cases}}_J \text{ contact @ J}$$

and the expression of dynamic screw

$$(\textcircled{2}) \quad \{\mathcal{d}\mathcal{H}\} = \begin{cases} mR(\ddot{\theta} \hat{v} - \dot{\theta}^2 \hat{u}) \\ 0 \end{cases}$$

$$\left\{ \mathcal{L}_{1/0} \right\} = \left\{ \frac{d}{dt} \dot{\theta} \right\}_{1/0} = \left\{ -\frac{2}{5} mrR(\ddot{\theta}\hat{u} + \dot{\theta}\hat{z}_0 - \theta\ddot{\hat{v}}) \right\}_C$$

we can immediately apply the FTD to obtain 6 equations.  
Note that we have 6 unknowns:  $\theta(t)$ ,  $N_I$ ,  $F_{Iu}$ ,  $F_{Ir}$ ,  $N_J$ ,  $F_J$ .

The resultant gives 3 equations on basis  $(\hat{u}, \hat{v}, \hat{z}_0)$ :

$$-mr\ddot{\theta}^2 = F_{Iu} - N_J \quad (5)$$

$$mr\ddot{\theta} = F_{Ir} + F_J \quad (6)$$

$$0 = N_I - mg \quad (7)$$

For the moment equation, we need to resolve the action screw about C:

$$\begin{aligned} M_{C, T+1} &= \underbrace{\underline{r}_{CI} \times (N_I \hat{z}_0 + F_{Iu} \hat{u} + F_{Ir} \hat{v})}_{-r \hat{z}_0} + \underbrace{\underline{r}_{CJ} \times (-N_J \hat{u} + F_J \hat{v})}_{r \hat{u}} \\ &= -r F_{Iu} \hat{v} + r F_{Ir} \hat{u} + r F_J \hat{z}_0 \end{aligned}$$

This gives 3 additional equations:

$$-\frac{2}{5}mrR\ddot{\theta}^2 = rF_{Ir} \quad (8)$$

$$\frac{2}{5}mrR\ddot{\theta}^2 = -rF_{Iu} \quad (9)$$

$$-\frac{2}{5}mrR\ddot{\theta}^2 = rF_J \quad (10)$$

**Q.5.**

$$\text{We take (8) + (10) to find } F_{Ir} + F_J = -\frac{1}{5}mrR\ddot{\theta}^2 \quad \Rightarrow \quad \ddot{\theta} = 0$$

$$\text{We also have (6): } F_{Ir} + F_J = mr\ddot{\theta}$$

$$\text{This shows that } \dot{\theta} = \dot{\theta}_0 \Rightarrow F_{Ir} = F_J = 0$$

$$(7) \Rightarrow N_I = mg$$

$$(9) \Rightarrow F_{Iu} = -\frac{2}{5}mrR\dot{\theta}_0^2$$

$$(5) \Rightarrow N_J = F_{Iu} + mr\dot{\theta}^2 = \frac{3}{5}mr\dot{\theta}_0^2 = N_J$$

Since  $N_I > 0$  and  $N_J > 0$  (if  $\dot{\theta}_0 \neq 0$ ), the sphere never loses contact @ I and J.

**Q.6**

For no-slip to be maintained, we need to impose

$$|F_{Ir}| < \mu N_I \quad \text{and} \quad |F_J| < \mu N_J$$

$|F_J| < \mu N_J$  and  $|F_{In}| < \mu N_I$

Since  $F_J = 0$ , the first condition is always satisfied.

Using  $F_{In} = -\frac{2}{5}mR\dot{\theta}_0^2$  and  $N_I = mg$ , we find the condition

$$\frac{2}{5}mR\dot{\theta}_0^2 < \mu mg \quad \text{or}$$

$$\dot{\theta}_0^2 < \frac{5\mu}{2}\frac{g}{R}$$